

# Modeling Active Vision During Smooth Pursuit of a Robotic Eye

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## Abstract

*The computational framework, based on the conformal camera, is developed for processing visual information during smooth pursuit movements of a robotic eye. During smooth pursuit, the image of the tracked object remains nearly stationary while the image of a stationary background sweeps across the image plane of the camera. The background's image transformation derived in the second-order approximation enable the anticipation of the perceptual outcome of the camera pursuit. This can be used to support the correct visual information of the moving object in front of the stationary background. These results complement the author's previous study on the predictive image processing for visual stability during the conformal camera movements resembling primate's saccadic eye rotations. The visual information processing algorithms that can support visual stability during smooth pursuit and saccadic movements of an anthropomorphic robotic camera are needed for an autonomous robot efficient interactions with the real world, in real time.*

## Introduction

In this article we develop a computational framework for biologically-mediated processing of visual information during foveated-sensor camera rotations resembling primate's smooth pursuit eye movements (SPEM). The presented algorithms can support perceptual stability for autonomous robotic systems needed for their efficient interaction with dynamic environments.

### Primate Perception During Eye Movements

Whenever primates direct the gaze to attend a scene detail, their highest acuity is confined to the foveal region subtending the visual angle of 2 degrees. To overcome the acuity limitation of foveated vision, humans and other primates explore the scene by making about 3 to 5 saccades per second with the eyeballs speed of up to 900 deg/s to fixate the high-acuity fovea on the salient and behaviorally relevant parts of the scene. In addition, primates are able to execute smooth pursuit eye movements that keep the fovea focused on a slowly moving object (up to 100 deg/s), but they also employ a combination of smooth pursuit and saccades to track an object moving unpredictably or moving faster than 30 deg/s).

Visual neurons in the primate brain have spatial receptive fields (RFs) that encode the position of an object in gaze-centered coordinates, that is, in respect to the frame centered on the fovea in retinotopic maps. Because of incessant eye movements, the retinotopic representation of this position information is constantly changing. For this reason, very sophisticated neural processes have evolved to maintain a temporally continuous, stable perception of the world.

The identification of visuosaccadic pathways [19] supports the idea that the brain uses a copy of the oculomotor command of the impending saccade, referred to as efference copy or corol-

lary discharge (see a review in [3], to shift transiently the RFs of stimuli to their future location before the eyes saccade takes them there. This shift remaps the retinotopic maps from the presaccadic frame to the postsaccadic frame in the anticipation of each upcoming saccade, giving access to the visual information at the saccadic target before the saccade is executed. It is believed that this predictive remapping mechanism contribute to visual stability [4, 11].

Smooth pursuit eye movements (SPEMs) by stabilizing the tracked objects image on the fovea, superimpose additional motion on the retinal images of the stationary background and other moving objects, leading to the possible distortion of the perceived speed and direction of motion. Moreover, in natural viewing corrective saccades often accompany smooth pursuit eye movement [2, 17]. Whenever eyes are pursuing a moving object in front of a stationary background, the object's image is stabilized on the fovea and the background image sweeps across the retina in opposite direction. Nevertheless, we generally perceive the object as moving and the background as stationary, despite opposite retinal information. This indicates that the stable perception that we enjoy has to be maintained at all time during SPEM. Consequently, in addition to the extraretinal information such as eye intended movement (efference copy), the retinal motion information should also contribute to processing visual information during smooth pursuit [7, 9, 13].

### Modeling Visual Information During Robotic Eye Movements

Visual information acquisition sensors, with software and/or hardware-implemented image processing used in anthropomorphic cameras, can be classified into two broad categories. The foveated-sensor, frame-based, video acquisition systems [1, 27] and asynchronous spiking, frame-less, contrast-variation acquisition systems [10, 16]. Frame-less based vision systems have a huge advantage over standard frame-based vision systems due to very high dynamic range and temporal resolution, but very low computational load and internal latency [14].

The frame-based cameras with foveated sensor architecture have been implemented in numerous applications in the context of machine vision, but they have not been widely used in commercial applications due to the lack of efficient tools for processing and analyzing visual information [28]. On the other hand, so far only a limited range of applications has been demonstrated for frame-less vision systems mainly because the visual information processing and analyzing tools are not available [5].

The conformal camera framework [23, 24] has been recently used in [25, 26] to model some of the front-end processes underlying stability of perception for a foveated-sensor camera head mounted on the moving platform that replicates human saccadic eye movements [6, 8]. In this study, the conformal camera's geometric framework is applied to develop anticipatory processing



and note that

$$h(b_1, b_2, b_3) \cdot z = \begin{bmatrix} \delta & \gamma\delta \\ 0 & 1/\delta \end{bmatrix} \cdot z.$$

The  $h$ -transformation is followed by the  $k$ -transformation that results from the rotation of the object by  $(\psi, \phi, \psi')$  relative to the center of projection  $N$ . That is, the image is first projected into the sphere  $S^2$  by  $\sigma^{-1}$ , then it is rotated with the sphere by the Euler angles  $(\psi, 2\phi, \psi')$  (here,  $\psi$  is the rotation angle about the  $x_3$ -axis, followed by the rotation angle  $2\phi$  about the  $x_2$ -axis and the rotation angle  $\psi'$  about the  $x_3$ -axis) and projected back to the image plane, giving

$$z'' = k(\psi, 2\phi, \psi') \cdot z' = \begin{bmatrix} \alpha & \beta \\ -\bar{\beta} & \bar{\alpha} \end{bmatrix} \cdot z' = \frac{\alpha z' + \beta}{-\bar{\beta} z' + \bar{\alpha}} \quad (6)$$

where

$$\alpha = e^{-i(\psi+\psi')/2} \cos \phi, \quad \beta = -e^{-i(\psi-\psi')/2} \sin \phi. \quad (7)$$

The composition of the  $h$ - and  $k$ -transformations gives the image  $g$ -transformation of an object undergoing rigid motions in the scene

$$z'' = g \cdot z = k(\psi, 2\phi, \psi') h(b_1, b_2, b_3) \cdot z. \quad (8)$$

### The Group of Image Projective Transformations

In this section we briefly describe the action of the group of projective transformations of the image intensity function and refer to [22, 23] for detailed discussion.

In the conformal camera, the image projective transformations are defined as the composition of finite iterations of the  $h$ - and  $k$ -transformations.

Then, by the representation of  $h$ - and  $k$ -transformations as the matrices acting on the points of the image plane, see (5), we obtain that the image projective transformations are given by the mappings

$$g \cdot z = \frac{az+b}{cz+d}, \quad g = \begin{bmatrix} a & b \\ c & d \end{bmatrix} \in \mathbf{SL}(2, \mathbf{C}), \quad (9)$$

which are extended to the Riemann sphere  $\hat{\mathbf{C}} = \mathbf{C} \cup \{\infty\}$  as follows:

$$\begin{aligned} \begin{bmatrix} a & b \\ c & d \end{bmatrix} \cdot \infty &= a/c, \quad \begin{bmatrix} a & b \\ c & d \end{bmatrix} \cdot (-d/c) = \infty, \quad \text{if } c \neq 0, \\ \text{and} \quad \begin{bmatrix} a & b \\ 0 & 1/a \end{bmatrix} \cdot \infty &= \infty. \end{aligned}$$

In (9)

$$\mathbf{SL}(2, \mathbf{C}) = \left\{ \begin{bmatrix} a & b \\ c & d \end{bmatrix} : ad - bc = 1 \right\},$$

is the group of  $2 \times 2$  matrices of complex numbers with determinant one.

For the given intensity function  $f(z)$ , its image projective transformations are given by

$$\begin{aligned} f(z) \mapsto f_g(z) &= f(g^{-1} \cdot z) = f\left(\frac{dz-b}{-cz+a}\right), \\ g &= \begin{bmatrix} a & b \\ c & d \end{bmatrix} \in \mathbf{SL}(2, \mathbf{C}). \end{aligned} \quad (10)$$

### Imaging with the Conformal Camera

The basic image transformations in the conformal camera can only be defined for the planar objects in the scene, cf. [23]. To justify this requirement, we note that only the most basic features are extracted from the impinged visual information on the retina before they are sent to the brain areas for processing. Thus, the initial image of the centrally projected scene is comprised of numerous brightness and color spots from many different locations in space, without explicit information about the perceptual organization of the scene [18]. What is initially perceived is a small number of objects' surfaces that are segmented from the background and from each other [15]. The object's 3D attributes are acquired when 2D projections on the retina are processed downstream the visual pathway by neuronal populations extracting the monocular information (texture gradients, relative size, linear and aerial perspectives, shadows and motion parallax) and, whenever disparity is also available (two eyes seeing the scene), the binocular information.

### Active Imaging: the Vector $\mathbf{b}$

We demonstrate in Fig. 3 that when the line of sight of the camera is rotated, the image transformation of a planar stationary object is given by the  $kh$ -transformation,

$$\begin{aligned} z' &= k(\psi, -2\phi, \psi') h(b_1, b_2, b_3) \cdot z \\ &= \begin{bmatrix} \alpha & \beta \\ -\bar{\beta} & \bar{\alpha} \end{bmatrix} \begin{bmatrix} \delta & \gamma\delta \\ 0 & 1/\delta \end{bmatrix} \cdot z \\ &= \frac{\alpha\delta^2 z + \alpha\gamma\delta^2 + \beta}{-\bar{\beta}\delta^2 z - \bar{\beta}\gamma\delta^2 + \bar{\alpha}}, \end{aligned} \quad (11)$$

where  $\delta = (1 - b_3)^{-1/2}$  (with  $b_3 < 1$ ),  $\gamma = b_1 + ib_2$  and  $\alpha$  and  $\beta$  are given in (7).

In fact, Fig. 3 explains that when the camera rotates by  $\phi$  about the  $x_2$ -axis, the center of projection undergoes translation by  $\mathbf{t} = N\bar{N}_1'$ . Then, the object both translates by  $-\mathbf{t}$  and rotates by  $-\phi$  with respect to the center of projection, the point  $N$  representing the eye's pupil.

In the image transformation (11), the eye's rotation angles can be assumed known, as they are used to program the eye movements. However, the vector  $\mathbf{b}$  is the model's internal parameter which has to be derived in terms of the eye's intended gaze change and object's geometry and location. In this section, the vector  $\mathbf{b}$  is obtained in a full generality.

Referring to Fig. 3, the coordinates of the object's endpoints  $P(p_3, p_1)$  and  $Q(q_3, q_1)$  are

$$p_1 = s \tan \phi, \quad p_3 = s + 1$$

where  $s$  is the distance to the fronto-parallel plane containing the endpoint  $P$  and

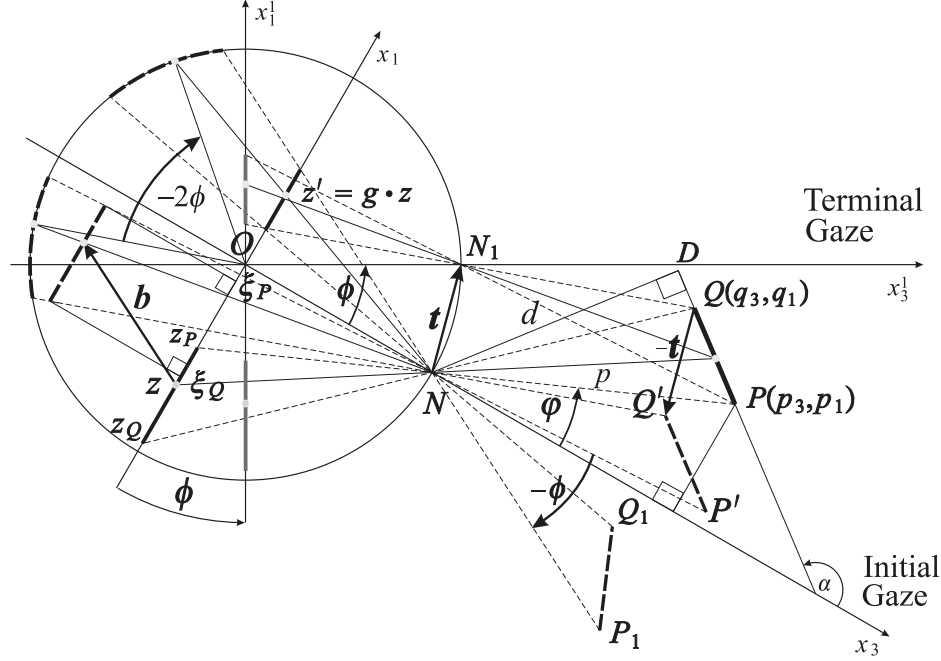
$$q_1 = s \tan \phi + w \sin \alpha, \quad q_3 = s + 1 + w \cos \alpha.$$

Because under the gaze rotation  $\phi$ , the center of projection  $N$  is translated by  $\mathbf{t}$ ,  $PQ$  is translated by the vector  $-\mathbf{t}$ , where

$$\mathbf{t} = \langle t_3, t_1 \rangle = \langle \cos \phi - 1, \sin \phi \rangle \quad (12)$$

Coordinates of the endpoints  $P'(p'_3, p'_1)$  and  $Q'(q'_3, q'_1)$  of the translated line segment  $P'Q'$ , are the following

$$p'_1 = s \tan \phi - \sin \phi, \quad p'_3 = s + 2 - \cos \phi$$



**Figure 3.** When the camera gaze is rotated by  $\phi$ , the image projective transformation in the initial coordinate system is given by the  $g$ -transformation where  $g = hk$  is the result of the composition of the relative object movements (translation by  $-\mathbf{t}$  and rotation by  $-\phi$  in the scene).

and

$$\begin{aligned} q'_1 &= s \tan \phi + w \sin \alpha - \sin \phi, \\ q'_3 &= s + 2 + w \cos \alpha - \cos \phi. \end{aligned}$$

The components  $b_1$  and  $b_3$  of the vector  $\mathbf{b}$  are derived from the relation,

$$b_1 = \xi_P - z_P = \xi_Q - z_Q \quad (13)$$

and the proportions obtained from similar triangles  $\triangle N z_P O \sim \triangle N P p_3$ ,  $\triangle N z_Q O \sim \triangle N Q q_3$ , and similar triangles that can be easily identified from the last two of the following proportions

$$\begin{aligned} \frac{-z_P}{1} &= \frac{p_1}{p_3 - 1}, \\ \frac{-z_Q}{1} &= \frac{q_1}{q_3 - 1} = \frac{s \tan \phi + \sin \alpha - \sin \phi}{s + 1 - \cos \phi}, \\ \frac{\xi_P}{1 - b_3} &= -\frac{p_1 - t_1}{p_3 - 1 - t_3} = -\frac{s \tan \phi - \sin \phi}{s + 1 - \cos \phi}, \end{aligned}$$

and

$$\frac{-\xi_Q}{1 - b_3} = \frac{q_1 - t_1}{q_3 - 1 - t_3} = \frac{s \tan \phi + w \sin \alpha - \sin \phi}{s + 1 + w \cos \alpha - \cos \phi}.$$

To this end, using the proportions in  $\xi_P - z_P = \xi_Q - z_Q$ , we first derive

$$\begin{aligned} & -\frac{(1 - b_3)(s \tan \phi + s \sin \phi)}{s + 1 - \cos \phi} + \tan \phi \\ &= -\frac{(1 - b_3)(s \tan \phi + w \sin \alpha - \sin \phi)}{s + 1 + w \cos \alpha - \cos \phi} \\ &+ \frac{s \tan \phi + w \sin \alpha}{s + w \cos \alpha} \end{aligned}$$

and then solve for  $b_3$ , to obtain

$$b_3 = 1 - \frac{\left(1 + \frac{1 - \cos \phi}{w \cos \alpha + s}\right) (s + 1 - \cos \phi)}{s + \frac{\tan \alpha (1 - \cos \phi)}{\tan \alpha - \tan \phi} + \frac{\sin \phi}{\tan \alpha - \tan \phi}} \quad (14)$$

Similarly, from  $b_1 = \xi_P - z_P$ , we have

$$b_1 = -\frac{\left(1 + \frac{1 - \cos \phi}{w \cos \alpha + s}\right) (s \tan \phi - \sin \phi)}{s + \frac{\tan \alpha (1 - \cos \phi)}{\tan \alpha - \tan \phi} + \frac{\sin \phi}{\tan \alpha - \tan \phi}} + \tan \phi, \quad (15)$$

where we substituted the expression for  $b_3$ .

## Sequence of Horizontal Gaze Rotations

Whenever eyes are pursuing a moving object, both eye movements and object movements induce an image motion on the retina. Therefore, eye movements must be compensated to allow a clear and stable perception of our surroundings. Given the complexity of the smooth pursuit system, the cortical processing of different coordinate systems (retinal information, information about object movement in space, and information about eye movement relative to the head) and the visual-to-motor transformations necessary to generate these precise eye movements remain largely unclear [20]. Hence, our goal here is to layout the geometric and computational framework for visual information processing during SPEM without assuming the neural mechanisms maintaining visual stability. In particular, we study the background image projective transformations that occur when the conformal camera's gaze is horizontally rotated.

### Linearization of the Vector $\mathbf{b}$

Introducing power series  $\sin \phi = \phi - \phi^3/6 + \dots$  and  $\cos \phi = 1 - \phi^2/2 + \dots$  into expressions for  $b_3$  and  $b_1$  given in (14) and (15),

where ‘..’ indicates the corresponding higher order terms in  $\phi$ , we get for (14),

$$b_3 = 1 - \frac{1 + \left(\frac{1}{s} + \frac{1}{w \cos \alpha + s}\right) \frac{\phi^2}{2} + \dots}{1 + \frac{1}{s(\tan \alpha - \tan \phi)} \phi + \dots},$$

which is expanded in powers of  $\phi$  as follows,

$$b_3 = \frac{1}{s(\tan \alpha - \tan \phi)} \phi - \left[ \frac{1}{w \cos \alpha + s} - \frac{\tan \phi}{s(\tan \alpha - \tan \phi)} - \frac{2}{s^2(\tan \alpha - \tan \phi)^2} \right] \frac{\phi^2}{2} + \dots$$

Similarly, for (15), we have

$$b_1 = - \frac{\tan \phi - \frac{1}{s} \phi + \frac{\tan \phi}{w \cos \alpha + s} \frac{\phi^2}{2} + \dots}{1 + \frac{1}{s(\tan \alpha - \tan \phi)} \phi + \frac{\tan \alpha}{s(\tan \alpha - \tan \phi)} \frac{\phi^2}{2} + \dots} + \tan \phi,$$

which is expanded as follows,

$$b_1 = \frac{\tan \alpha}{s(\tan \alpha - \tan \phi)} \phi - \left[ \frac{\tan \phi}{w \cos \alpha + s} - \frac{s \tan \phi \tan \alpha - 2}{s^2(\tan \alpha - \tan \phi)} - \frac{2 \tan \phi}{s^2(\tan \alpha - \tan \phi)^2} \right] \frac{\phi^2}{2} + \dots$$

Then, substituting

$$s(\tan \alpha - \tan \phi) = \frac{s \sin(\alpha - \phi)}{\cos \alpha \cos \phi} = \pm \frac{d}{\cos \alpha}$$

where  $d$  is the distance to the plane containing the planar object,

$$d = \frac{s |\sin(\alpha - \phi)|}{\cos \phi}, \quad (16)$$

which can be easily obtained from the right triangle  $\triangle NDP$  in Fig. 3, we arrive at the second order approximations

$$b_3 \approx \pm \frac{\cos \alpha}{d} \phi - \left[ \frac{1}{w \cos \alpha + s} \pm \frac{\sin \alpha}{d} + \frac{2 \cos^2 \alpha}{d^2} + \frac{1}{s} \right] \frac{\phi^2}{2} \quad (17)$$

$$b_1 \approx \pm \frac{\sin \alpha}{d} \phi + \left[ -\frac{\tan \phi}{w \cos \alpha + s} \pm \frac{s \tan \phi \sin \alpha - 2 \cos \alpha}{sd} - \frac{2 \tan \phi \cos \alpha^2}{d^2} \right] \frac{\phi^2}{2} \quad (18)$$

that make the set of parameters especially convenient for error analysis. In the above expressions, the upper sign is for  $\alpha > \phi$  while the lower sign is for  $\alpha < \phi$ .

Thus, the approximation of vector  $\mathbf{b}$  to the first order in  $\phi$  is the following

$$\mathbf{b} = \pm \frac{\phi}{d} \langle \cos \alpha, \sin \alpha \rangle. \quad (19)$$

where  $\alpha$  gives the orientation of the object  $PQ$  relative to the initial coordinate system and  $d$  is the distance (16) to the plane containing the (planar) object.

From the second order terms in (17) and (18), we see that the approximation breaks down when  $\alpha = \phi$  or  $\alpha = \phi \pm \pi$ , and when

$\phi = \pm \pi/2$ . From (16) and  $s = p \cos \phi$ , where  $p$  is the distance to  $P$  satisfying  $p \neq 0$ , we see that  $s = 0$  if and only if  $\phi = \pm \pi/2$ , and  $d = 0$  if and only if  $\alpha - \phi = 0, \pm \pi$ . Under the first condition ( $s = 0$ ), some points do not project to the image plane (that is, they project to  $\infty$ ), and under the second condition ( $d = 0$ ), a planar two-dimensional object has a one-dimensional projection on the image plane. These conditions are the same as the ones that prevent the proper functioning of the primate vision system.

Maybe the most significant result is the fact that in the first order approximation, the vector  $\mathbf{b}$  direction (relative to the initial coordinate system) is given by the angle  $\alpha$  ( $\mathbf{b}$  is parallel to  $\overrightarrow{PQ}$ ), while its length depends linearly on  $\phi$  (or  $-\phi$ ) and inversely on  $d$ , the distance to the plane containing the planar object.

Thus, since the values of  $\alpha$  and  $d$  fix the plane containing the planar object, the leading term approximation of  $\mathbf{b}$  does not depend on the object size  $w$  or where on the plane it is located. We conclude that the approximation (19) applies directly to 2D planar objects (or planar surfaces of 3D objects) as it does not depend on the shape of these objects.

### Sequence of Small Gaze Rotations

We consider a sequence of horizontal rotations ( $\phi_m, m = 1, 2, 3, \dots$ ), where  $\phi_m$  is the angle rotating gaze  $m - 1$  to gaze  $m$  with the 0th gaze being the initial gaze. The image transformations are given in the initial coordinate system.

From now on, we change to the following notation: the coordinate system rotated with the camera by the angle  $\phi_m$  is denoted by  $(x_3^m, x_1^m)$ . We choose both  $\phi_m$  and the scene parameters, such that the corresponding image  $h$ -transformation is well approximated by using the linear term of the vector  $\mathbf{b}_m$ ,

$$\mathbf{b}_m = \frac{\phi_m}{d_{m-1}} \langle \cos \beta_{m-1}, \sin \beta_{m-1} \rangle. \quad (20)$$

Here, for  $m = 1$ ,  $d_0 = d$  and  $\beta_0 = \alpha$ , so that

$$\mathbf{b}_1 = \frac{\phi_1}{d} \langle \cos \alpha, \sin \alpha \rangle. \quad (21)$$

We need to find  $\beta_m$  and  $d_m$  for  $m \geq 2$ . To this end, when the conformal camera undergoes the second gaze rotation  $\phi_2$ , the angle  $\beta_2$  of  $\mathbf{b}_2$  is  $\alpha - \phi_1$ .

Thus, for the  $m$ th gaze rotation, the angle  $\beta_{m-1}$  of  $\mathbf{b}_m$  is the following

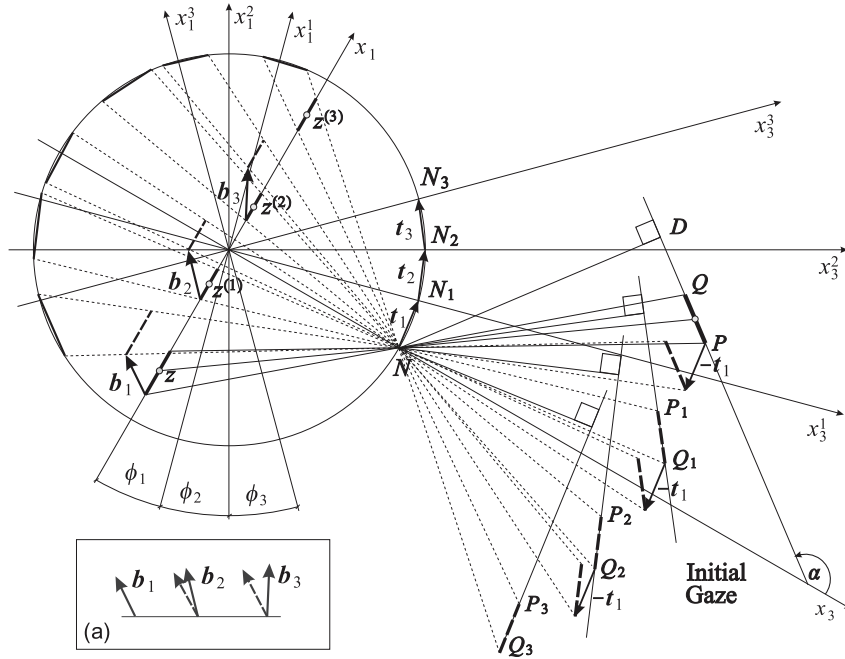
$$\beta_{m-1} = \alpha - \sum_{k=1}^{m-1} \phi_k, \quad m \geq 2. \quad (22)$$

Finally, using the results derived in Appendix, we have the following formulas for  $d_m$ ,

$$\begin{aligned} d_{m-1} &= \pm d + 2 \sin \left[ \frac{1}{2} \sum_{k=1}^{m-1} \phi_k \right] \cos \left[ \alpha - \frac{1}{2} \sum_{k=1}^{m-1} \phi_k \right] \\ &= \pm d + \sin \alpha - \sin \beta_{m-1}, \quad m \geq 2 \end{aligned} \quad (23)$$

with the upper sign holding for  $\alpha > \phi$  and the lower sign holding for  $\alpha < \phi$ . The distance  $d$  is given in (16).





**Figure 4.** The image projective transformations during the sequence of the gaze rotations  $\phi_1$ ,  $\phi_2$  and  $\phi_3$ . The relative motions of the object  $PQ$  used in the construction of the image transformations, as explained in Fig. 3, are also shown. The panel (a) confirms the results from the previous section on the approximation of the vector  $\mathbf{b}$  in (20) and (22): the direction of  $\mathbf{b}_2$  is the rotated direction of  $\mathbf{b}_1$  by  $\phi_1$ , and the direction of  $\mathbf{b}_3$  is the rotated direction of  $\mathbf{b}_1$  by  $\phi_1 + \phi_2$

## Conclusions: Modeling Horizontal SPEM

The horizontal SPEM with angular speed  $\omega(t)$ ,  $t \geq a$  is approximated for a time step  $\Delta t$  by a sequence of discrete rotations ( $\phi_m, m = 1, 2, 3, \dots$ ) where  $\phi_m = \omega_m \Delta t$  is the rotation from gaze  $m-1$  to gaze  $m$  with the average angular speed  $\omega_m$  in time interval  $[t_{m-1}, t_m]$ ,  $t_m = a + m\Delta t$ . For  $\omega(t)$  we choose  $\Delta t$  such that for each  $\phi_m$ , the approximation (20) holds.

Let the intensity function  $f(z)$  denote the image of the object. Using the results from the previous section and Fig. 4, the image projective transformation of the rotation from gaze  $m-1$  to gaze  $m$ , in the initial coordinate system, is the following

$$f(z^{(m-1)}) \mapsto f(z^{(m)}) = f(g_m^{-1} \cdot z^{(m-1)}), \quad (24)$$

where

$$\begin{aligned} g_m &= k(0, -2\phi_m, 0) h(b_m \sin \beta_{m-1}, 0, b_m \cos \beta_{m-1}) \\ &= \begin{bmatrix} \cos \phi_m & \sin \phi_m \\ -\sin \phi_m & \cos \phi_m \end{bmatrix} \begin{bmatrix} \delta_m & \gamma_m \delta_m \\ 0 & 1/\delta_m \end{bmatrix} \end{aligned} \quad (25)$$

and hence,

$$\begin{aligned} g_m^{-1} &= h^{-1}(b_m \sin \beta_{m-1}, 0, b_m \cos \beta_{m-1}) k^{-1}(0, -2\phi_m, 0) \\ &= \begin{bmatrix} 1/\delta_m & -\gamma_m \delta_m \\ 0 & \delta_m \end{bmatrix} \begin{bmatrix} \cos \phi_m & -\sin \phi_m \\ \sin \phi_m & \cos \phi_m \end{bmatrix} \end{aligned} \quad (26)$$

Here  $b_m = \phi_m / d_{m-1}$  and  $\beta_{m-1}$  and  $d_{m-1}$  are given in (22) and (23), respectively. Further,  $\delta_m = (1 - b_m \cos \beta_{m-1})^{-1/2}$  and  $\gamma_m = b_m \sin \beta_{m-1}$ . In implementation, the product of matrices in (26) has to be linearized in  $\phi_m$ .

By the iteration of (24) we obtain the SPEM's sequence of image projective transformations of the object given only in terms

of the initial orientation angle  $\alpha$  and the distance  $d$  of the plane containing the object planar surface.

Explicitly, for the given initial image  $f$  of a stationary object and the given SPEM's sequence ( $\phi_1, \phi_2, \dots, \phi_n$ ), the image undergoes the following transformation under the pursuit

$$f(z^{(n)}) = f(g_{(n,n-1,\dots,1)}^{-1} \cdot z)$$

where  $g_{(n,n-1,\dots,1)} = g_n g_{n-1} \dots g_2 g_1$  and

$$g_{(n,n-1,\dots,1)}^{-1} = g_1^{-1} g_2^{-1} \dots g_{n-1}^{-1} g_n^{-1}$$

with  $g_m^{-1}$  given in (26).

We recall that each  $d_{m-1}$  in (23), which describes the vector  $\mathbf{b}_m$  in (20), can be determined only by the planar object (or planar surface of the object) orientation  $\alpha$  and the distance  $d$  to the plane containing this object. These values can be typically estimated by the primate's vision system. Therefore, our modeling of the SPEM with the conformal camera should be able to support the stability of visual informations during smooth pursuit of an anthropomorphic robotic camera that is needed for an autonomous robot efficient interaction with the real world, in real time.

Implementation in a pursuit movement by the conformal camera will be done in the future.

## Appendix: The Formula For $d_m$

In this appendix we derive the formula for  $d_m$  that appeared in (20). To get  $d_m$ , we use Fig. 5 which shows details near projection centers  $N_1, N_2$  and  $N_3$  of the three first gaze rotations gaze rotations  $\phi_1, \phi_2$  and  $\phi_3$ .

To this end, using the isosceles triangle  $\triangle CNN_k$  and the fact that  $|CN| = 1$ , we first note that

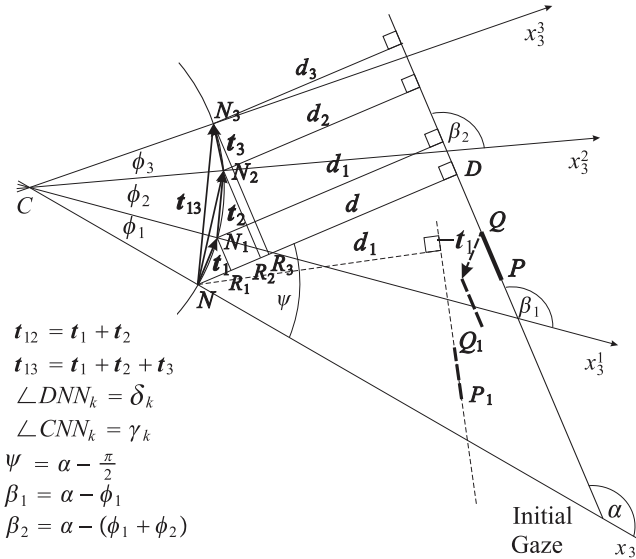


Figure 5. Geometric details near the projection centers  $N$  and  $N_1$  shown in Fig. 3 and the next two projection centers  $N_2$  and  $N_3$ .

$$\begin{aligned}
 |\mathbf{t}_{1m}| &= |\mathbf{t}_1 + \mathbf{t}_2 + \dots + \mathbf{t}_m| \\
 &= 2 \sin \left[ \frac{1}{2} (\phi_1 + \phi_2 + \dots + \phi_m) \right] \\
 &= 2 \sin \left[ \frac{1}{2} \left( \sum_{k=1}^m \phi_k \right) \right]
 \end{aligned}$$

and

$$\gamma_m = \frac{\pi}{2} - \frac{1}{2} \sum_{k=1}^m \phi_k.$$

Next, at the vertex  $N$ , we can write

$$\psi + \delta_m + \gamma_m = \pi$$

which, using  $\psi = \alpha - \pi/2$ , can be solved for  $\delta_m$  as follows

$$\delta_m = \pi - \alpha + \frac{1}{2} \sum_{k=1}^m \phi_k.$$

Finally, from

$$\begin{aligned}
 d - d_m &= |NR_m| = |\mathbf{t}_{1m}| \cos \delta_m \\
 &= 2 \sin \left[ \frac{1}{2} \sum_{k=1}^m \phi_k \right] \cos \left[ \pi - \alpha + \frac{1}{2} \sum_{k=1}^m \phi_k \right] \\
 &= -2 \sin \left[ \frac{1}{2} \sum_{k=1}^m \phi_k \right] \cos \left[ \alpha - \frac{1}{2} \sum_{k=1}^m \phi_k \right],
 \end{aligned}$$

which can be easily verified in Fig. 5, we obtain

$$\begin{aligned}
 d_m &= d + 2 \sin \left[ \frac{1}{2} \sum_{k=1}^m \phi_k \right] \cos \left[ \alpha - \frac{1}{2} \sum_{k=1}^m \phi_k \right] \\
 &= d + \sin \alpha - \sin \left[ \alpha - \sum_{k=1}^m \phi_k \right].
 \end{aligned}$$

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## Author Biography

*Jacek Turski was awarded his Ph.D. from McGill University. After holding postdoctoral positions at the University of Manitoba and the University of Houston, he joined the University of Houston-Downtown where he is now a Full Professor in the Department of Mathematics and Statistics. Within the geometric analysis framework of the conformal camera (the Riemann sphere), he has been modeling visual information during the foveated-sensor camera rotations resembling saccadic and smooth pursuit eye movements. His latest study, which will appear in Vision Research, corrects the two century-old Vieth-Müller model of the geometric horopter. That model, which is still influencing theoretical research in binocular vision, assumes that the optical node coincides with the eye rotation center, an anatomically incorrect location. Dr. Turski's research has been supported by NSF grants and has been published in mathematics, computer science and robotics journals.*